



TECHNICAL NOTES on Brick Construction

1850 Centennial Park Drive, Suite 301, Reston VA 20191 | www.gobrick.com | 703-620-0010

Technical Notes 43 - Passive Solar Heating with Brick Masonry - Part 1 Introduction June 1981

Abstract: Brick masonry passive solar energy systems can be used to significantly reduce the use of fossil fuels for heating and cooling buildings. The basic concepts and necessary considerations for the design of passive solar heating systems are discussed. The basic concepts involve the incorporation of the passive solar heating system into the architectural design of the intended use and operation of the building. Consideration of environmental factors is also discussed.

Key Words: attached sunspaces, bricks, buildings, cavity wall systems, climatology, conservation, direct gain systems, energy, masonry, passive solar heating systems, solar radiation, system operation, thermal storage walls.

INTRODUCTION

Energy conservation and fuel consumption have become a major concern in recent years. Much of the nation's fuel is used in the heating of buildings. The use of solar heating systems will help to reduce this consumption of non-renewable energy resources. Solar energy is an immediately available renewable energy source. Most buildings can easily be designed to benefit from solar heating.

Two types of solar energy systems may be used to heat buildings, active and passive. Active solar heating systems are those which require mechanical equipment for operation. Pumps and other mechanical devices are required to circulate liquids or gases through solar collectors, to storage media, and then to transfer the collected heat to the occupied spaces of the building.

Passive solar heating systems do not require the use of mechanical equipment. The heat flow in passive solar heating systems is by natural means: radiation, convection, and conductance. The thermal storage is in the structure itself. Although passive solar heating systems do not require mechanical equipment for operation, this does not mean that fans or blowers may not, or should not, be used to assist the natural flow of thermal energy. The passive systems assisted by mechanical devices are referred to as "hybrid" heating systems.

Passive solar systems utilize basic concepts incorporated into the architectural design of the building. They usually consist of: buildings with rectangular floor plans, elongated on an East-West axis; a glazed South-facing wall; a thermal storage media exposed to the solar radiation which penetrates the South-facing glazing; overhangs or other shading devices which sufficiently shade the South-facing glazing from the summer sun; and windows on the East and West walls, and preferably none on the North walls. Passive solar systems do not have a high initial cost or long-term payback period, both of which are common with many active solar heating systems.

This *Technical Notes* introduces the general features and requirements for the development and application of passive solar heating systems. Passive solar cooling systems are discussed in *Technical Notes* 43C. Due to the variations in building type and environment which must be considered, it is not normally feasible for passive solar systems to be the sole source of heat in most climatological areas. Construction details are provided in *Technical Notes* 43G.



Passive Solar Building with Thermal Storage Wall Under Construction

FIG. 1



Combined Thermal Storage Wall System and Attached Sunspace

FIG. 2

ENVIRONMENTAL DATA AND REQUIREMENTS

Many environmental factors must be considered to fully utilize the concepts of passive solar heating systems. Environmental data is given in Tables 1 and 2 of this *Technical Notes*.

Temperature

Exterior design temperatures are important considerations in developing passive solar heating systems. The size of the system will depend upon daily, monthly and annual temperature fluctuations. In mild, sunny climates, the required glazing and thermal storage areas may be relatively small. In temperate, cloudy climates, the required glazing area may be small, but the thermal storage requirements may be greater. In colder climates, the amount of glazing and thermal storage is usually large.

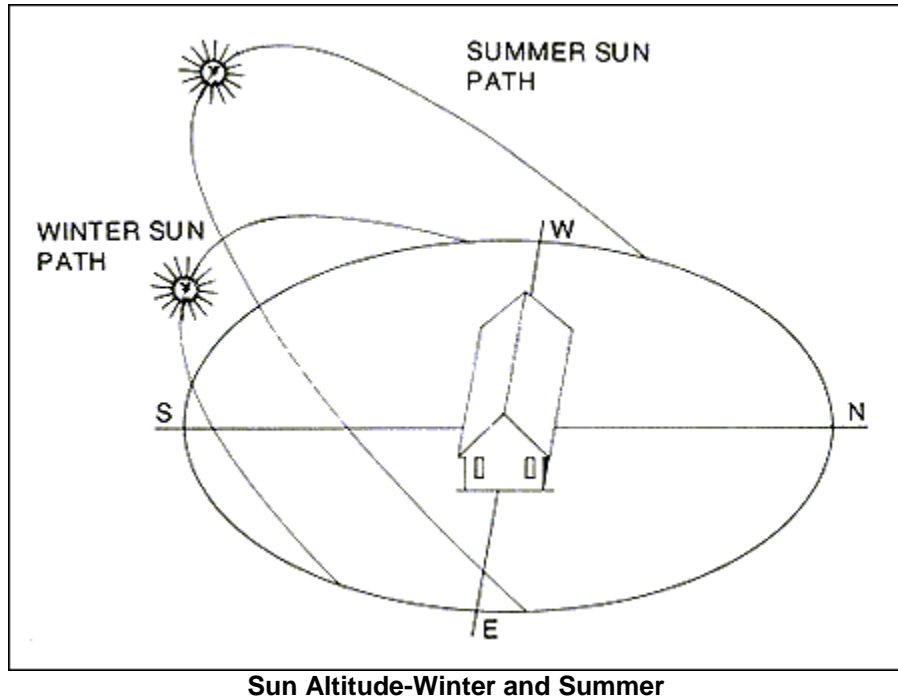
The average monthly heating degree days are related to exterior temperature conditions. These values are necessary to determine the total monthly thermal load of the building. Average monthly heating degree days and exterior temperatures are given in Table 2 at the end of this *Technical Notes*.

Latitude

Latitude is important to determine the amount of solar radiation and the appropriate summertime shading provided by overhangs and other devices. The further North the building is to be located, the less winter solar radiation it will receive. This is because the sun is above the horizon for a shorter period of time and the solar radiation must penetrate more of the atmosphere. Values of solar radiation at various latitudes are given in Table 1.

At higher latitudes, the sun appears lower in the sky. At these latitudes, where the position (altitude) of the sun in the sky is low, larger overhangs are required to shade the South-facing wall from the summer sunlight. Figure 3 shows how the altitude of the sun changes from winter to summer, demonstrating how the South-facing wall may

be shaded from summer solar radiation and still be exposed to winter solar radiation by using an overhang. The length of projection required to shade a South-facing wall from the summer sun is given in Table 3.



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bProjection greater than 20 ft required.

Solar Radiation Data

Solar radiation data is required to determine the amount of radiation transmitted through the South-facing glazing. Actual average solar radiation data for various geographical locations is given in Table 2. The amount of solar radiation is dependent on climate, elevation and latitude. Clear day solar radiation for various latitudes is given in Table 1.

Orientation

Orientation is extremely important in the design of passive solar buildings. The best performance will usually result when the passive solar system faces true South. True South may be obtained from isogonic (magnetic variation) charts developed by the United States Department of Commerce, Coast and Geodetic Survey, or by consulting a local land surveyor.

When the passive solar system faces true South, the system will be exposed to the maximum amount of winter solar radiation. Deviations of more than 30° East or West of true South are *not* recommended, especially where maximum performance is desired.

Site Topography

The topography of the site is of major concern. If the South-facing wall of the building is shaded by natural or man-made elements, it will probably not be feasible to consider passive solar systems. An ideal siting for a passive solar building is to be bermed into a South-facing slope. This provides a South wall exposed to the sun, and a North wall protected from environmental changes by the earth berm. Berming the North wall of the building should be done cautiously to avoid problems caused by ground water and earth pressure.

BUILDING TYPE AND USE

In addition to environmental considerations building type and use are very important in developing and applying passive solar heating systems. Building type and use are flexible requirements which allow the designer to make appropriate adaptations to the structure to provide the desired energy performance.

Thermal Load Requirements

Thermal load requirements are important in the selection and sizing of passive solar heating systems. The effects of building type and use on the thermal load are determined by the interior design temperature and the allowable temperature fluctuation. A warehouse may not require the same interior design temperature as a residential structure. Many commercial buildings are only occupied during daylight hours and do not have to maintain the higher interior working hour temperatures overnight. In many applications, the passive solar heating systems may provide similar performance as conventional heating systems with night-time setbacks.

Another aspect which affects the requirements of the building's use is human comfort. Passive solar systems provide conditions which contribute to human comfort. The brick storage areas of the system are warm. When surrounded by warm surfaces, the human body receives radiation from the warm surfaces. This permits the occupants to feel comfortable at lower interior air temperatures because heat is radiated *to* the body rather than *from* the body.

Glazing and Lighting Quality

The amount of natural lighting required will affect the selection of the type of passive solar heating system. Fabrics and even the glazing material itself may suffer from ultraviolet degradation when exposed to direct sunlight. In applications such as studios, admitting large quantities of diffuse solar radiation provides appropriate lighting.

The amount of glazing for most conventional structures is typically determined by the need or desire to provide contact with the exterior or to meet building code egress requirements. This is not usually a primary design consideration for the passive solar heating system

Material Properties

Massive brick masonry is recommended for thermal storage because of its inherent ability to store heat. Typically, brick exposed to direct sunlight should be of a dark color wherever it is to perform as a thermal storage media. The American Society of Heating, Refrigerating and air-conditioning Engineers (ASHRAE) defines dark colors as dark blue, red, brown and green. The properties of brick as related to passive solar applications are discussed in *Technical Notes* 43D.

System Operation

Passive solar heating systems may be shaded from the summer sun by fixed, adjustable or removable shading devices. Adjustable or removable overhangs or shading devices require operation, but permit the optimum use of the winter sun and can completely eliminate any solar exposure on the South-facing glass in the summer.

The performance of passive solar systems may be greatly enhanced by the use of night insulation. The insulation may be applied on the interior in the form of drapes or panels. Insulation may also serve as reflector panels or shading devices. Reflector-insulating panels may be hinged at the base of the South-facing glazing so that, when opened during the day, they reflect additional solar radiation through the glazing and when closed, provide night insulation. Night insulation may be operated manually or automatically.

Building Design and Appearance

There is no reason for passive solar heating systems to have an extremely unconventional design or appearance. The only required variations are: additional South-facing wall glazing, reduced glazing on the East and West walls, and preferably no glazing on the North wall; sufficient overhang or some other shading device to prevent the South-facing glazing from being exposed to the summer sun; and interior brick masonry. The interior brick masonry exposed to direct sunlight is used as the thermal storage component of the passive solar energy system. Additional interior brick masonry unexposed to direct sunlight is used to provide a thermal flywheel which reduces interior temperature fluctuations.

Spatial Requirements

The spatial requirements may dictate the type of system used. The depth of penetration of solar radiation into the structure may affect the system type selected. Buildings should be arranged with a longitudinal East-West orientation to maximize the solar exposure of the South-facing glazing. This minimizes the distance from the South wall to the North wall, across which the thermal energy from the passive solar energy system has to be distributed. Building energy performance may be increased by heating the North wall with solar radiation entering through the South-facing glazing.

DIRECT GAIN SYSTEMS

The direct gain system is simple and often used. The system consists of South-facing glazing which allows winter sunlight to enter the habitable spaces of the building. This thermal energy is stored in brick floors and walls. A schematic of a direct gain system is shown in Fig. 4. The South-facing glazing may be windows (operable or fixed), or glass doors. The brick masonry exposed to the solar radiation should generally be a dark color and 4 to 8 in. thick. All walls or other components not exposed to solar radiation should have light-colored surfaces.

In the direct gain system, the South-facing glazing permits sunlight to strike the brick masonry construction. The brick masonry, because of its color, mass and thermal properties, provides the thermal storage for the system. The brick masonry absorbs the thermal energy from the sunlight striking its surface. The heat, which is stored during the daylight hours, is released gradually. The heat that is reflected from the brick masonry provides heat to the habitable space during the daylight hours. The light-colored surfaces reflect the heat radiated or reflected from the brick masonry to the air and surroundings in the habitable space. If large amounts of heat are required during the daytime hours and less during night-time hours, this may be accomplished by using lighter colors of brick masonry.

Direct gain systems provide rapid temperature increases in the habitable space and may have large temperature fluctuations. This is because such systems often must be designed to prevent overheating. The systems may have limited amounts of brick masonry exposed to the winter sunlight. This is especially true in the lower latitudes where the winter sun has a higher altitude. This may be overcome by providing clerestories to obtain solar radiation on the North wall, as shown in Fig. 4.

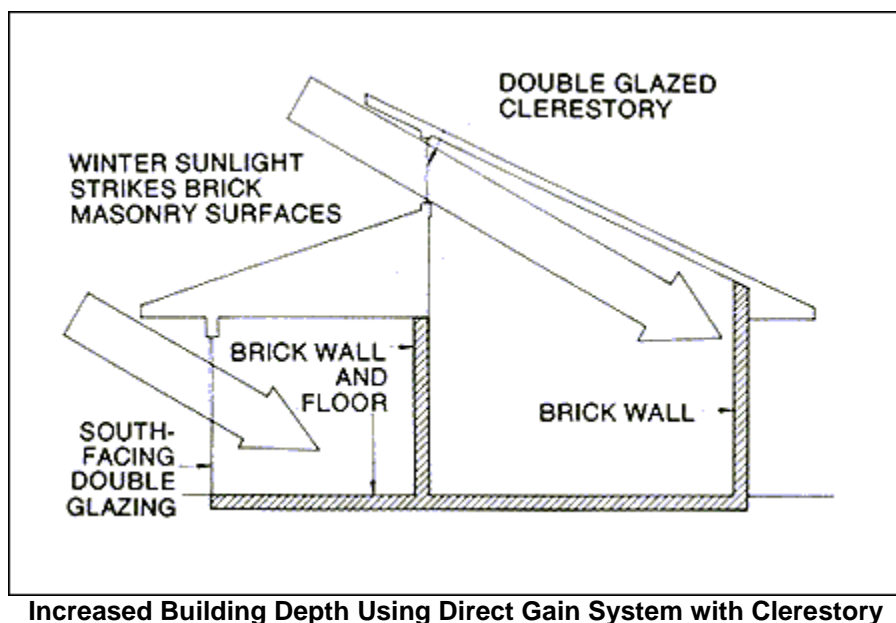


FIG. 4

Ultraviolet degradation is of the greatest concern when direct gain systems are utilized. Materials subject to ultraviolet degradation should not be exposed to direct sunlight. This may become an inconvenience in the living areas heated by direct gain. The walls and floors exposed to the sunlight and used for thermal storage should not be covered. Wall hangings and carpet greatly decrease the performance of the system.

THERMAL STORAGE WALL SYSTEMS

The thermal storage wall system, often referred to as a Trombe Wall System, is schematically represented in Fig. 5. The thermal storage wall may be vented, as shown in Fig. 5, and provide heat by radiation and convection, or it may be unvented and supply heat by radiation alone. A thermal storage wall system is shown on the left of Fig. 2. It consists of glazing, usually spaced 2 to 4 in. on the exterior of a South-facing wall, constructed of brick masonry. The massive brick wall, usually 10 to 18 in. thick, may be loadbearing, or non-loadbearing.

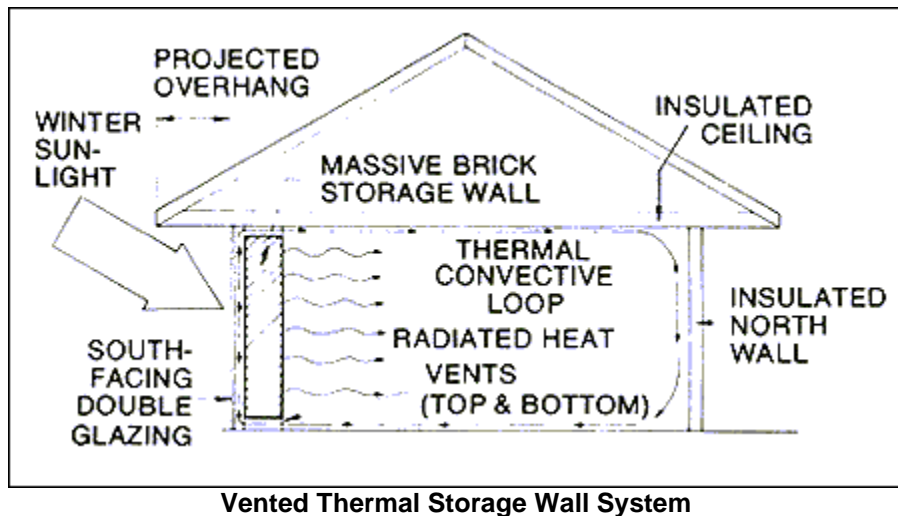


FIG. 5

The winter sunlight penetrating the South glazing heats the brick, the heat slowly penetrates the brick wall and warms the interior. Thermal storage walls may have sufficient heat storage to maintain comfortable temperatures in buildings for periods up to three completely overcast days. The thermal storage wall systems have considerably less temperature fluctuation than do direct gain systems, but usually do not achieve the same high initial interior temperatures.

The massive brick thermal storage wall prevents ultraviolet degradation of materials contained in the living space because solar radiation does not directly enter the habitable space. The performance may be substantially increased by providing vents at the top and bottom of the brick wall to provide convection in addition to the heat radiated from the interior face of the wall. Vented walls may be used to decrease the temperature fluctuations and increase the maximum temperature achieved in the living space. Fig. 1 shows a vented thermal storage wall under construction. When venting the storage wall system, vents with automatic or manual closures should be used so that the system does not reverse at night, creating a heat loss.

If controlled vents are not installed on the vented thermal storage wall systems, night insulation is essential to prevent heat losses at night. Night insulation may be required on unvented thermal storage walls and those with controlled vents to increase the efficiency of the system.

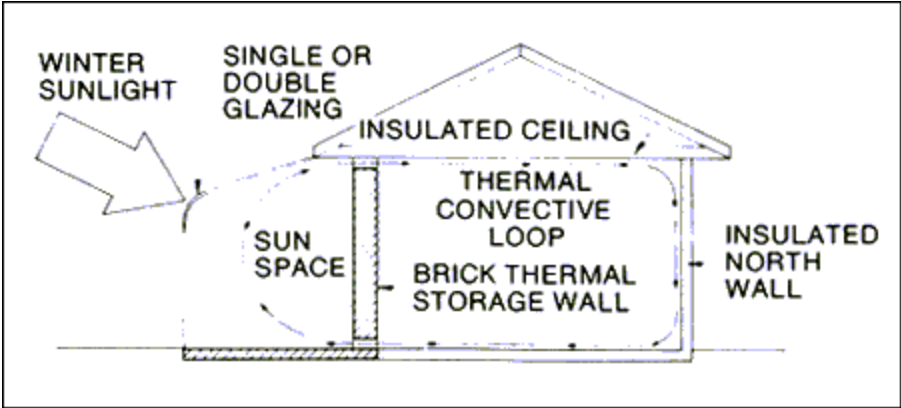
COMBINED SYSTEMS

The best thermal performance and living conditions result by combining the thermal storage wall system and the direct gain system. This combination permits some direct sunlight into the living spaces, achieves higher interior temperatures than the thermal wall system alone, provides less temperature fluctuation than the direct gain system alone and provides natural lighting. The combination essentially utilizes the best of the two systems.

ATTACHED SUNSPACES

Attached sunspaces are a combination of the components of the direct gain system and the thermal storage wall system, as shown in Fig. 2 on the right, and in Fig. 6. The sunspace is a room, or space, which typically has both a glass roof and a glass South-facing wall. The East and West walls may also be glass. The floor is similar to that of the direct gain system. It consists of 4 to 8-in. thick brick masonry. The North wall is a 10 to 18-in. thick brick thermal storage wall. The room is vented or ducted to other areas of the structure. With the assistance of fans and

blowers, the structure is heated by the extreme temperatures achieved in the sunspace. The sunspace usually has severe temperature fluctuations and is often unbearably hot during daylight hours. They do require removable shading devices to prevent solar gains in the summer. They will also require night insulation if they are to become useable living space in the evening hours.



Attached Sunspace

FIG. 6

CAVITY WALL SYSTEM

The cavity wall system, shown in Fig. 7, is a modification of the double envelope system. The concept of the cavity wall system is that the South-facing thermal storage wall heats up and creates a convective loop around the entire building envelope. The warmed air space minimizes the temperature differential from the interior of the building through the inner wythe of the cavity wall. There are no generally accepted design procedures for this type of system presently available. Some experts in the passive solar design field feel that the increased thermal

performance may be accounted for by the insulation in the interior and exterior shells of the double envelope system. Others feel that there is no convective loop occurring, i.e., the air between the double envelope shells is stagnant.

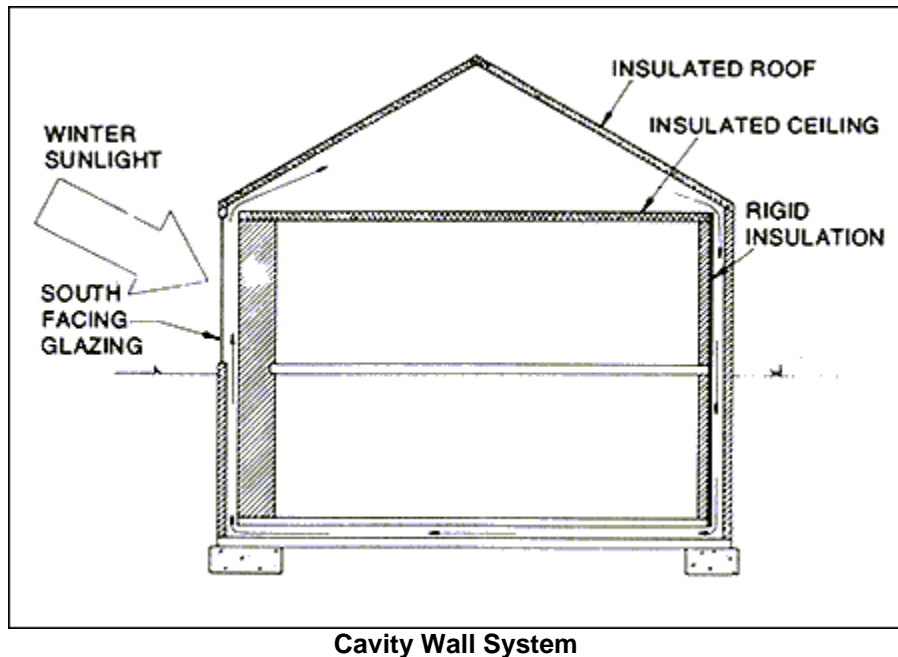


FIG.7

The use of a properly constructed, insulated brick cavity wall on the North side of the building could be used to provide a moderate heat loss to drive the convective loop through the air space in the building envelope. This would reduce the temperature of the air being circulated through the cavity, but the air should still reach high enough temperatures as it passes through the air space of the thermal storage wall system to provide a net heat gain.

Since there is still considerable controversy regarding this type of system, and since accurate performance analysis is not easily accomplished, these systems should only be designed and constructed with the appropriate awareness of the expected and achievable performance level of the system.

METRIC CONVERSION

Because of the possible confusion inherent in showing dual unit systems in the calculations, the metric (SI) units are not given in this *Technical Notes*. Table 13 in *Technical Notes 4* provides metric (SI) conversion factors for the more commonly used units.

SUMMARY

This *Technical Notes* has provided general information concerning passive solar heating systems. It has described several passive solar heating systems, the basic principles of their operation and general design consideration. This introduction to passive solar heating systems hopefully provides sufficient familiarization with concepts so that the design of such systems will be understood. Passive solar cooling is discussed in *Technical Notes 43C*. The material properties of brick masonry, as related to passive solar energy systems, is provided in *Technical Notes 43D*. Details and construction information are provided in *Technical Notes 43G*.

This *Technical Notes* does *not* and is *not* intended to provide information for specific designs and applications, but rather offers general information to assist in the consideration and use of brick masonry in passive solar heating systems. The decision to use these concepts in the design specific applications is *not* within the purview of the Brick Institute of America, and must rest with the owner or designer of any specific project.

Month	Normal Temperature (Deg F) ¹			Normal Degree Days ²	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F) ¹			Normal Degree Days ²	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F) ¹			Normal Degree Days ²	Total Hemispheric Mean Daily Solar Radiation
	Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly		
ALABAMA						ALABAMA (continued)						ALASKA					
Birmingham Latitude 33° 34' N Elevation 630'						Mobile Latitude 30° 41' N Elevation 220'						Fairbanks Latitude 64° 49' N Elevation 453'					
JAN	54.3	34.1	44.2	654	706.6	JAN	61.1	41.3	51.2	451	828.2	JAN	-2.2	-21.6	-11.9	2384	30.1
FEB	57.7	36.1	46.9	517	967.1	FEB	64.1	43.9	54.0	337	1099.6	FEB	9.3	-14.3	-2.5	1890	221.4
MAR	64.8	41.8	53.3	389	1296.1	MAR	69.5	49.2	59.4	221	1407.5	MAR	23.3	-4.3	9.5	1720	674.2
APR	75.3	51.0	63.2	116	1673.5	APR	78.0	57.7	67.9	40	1721.7	APR	40.4	17.3	28.9	1083	1193.9
MAY	82.5	58.4	70.5	20	1856.9	MAY	85.0	64.5	74.8	0	1872.1	MAY	58.8	35.7	47.3	549	1603.6
SEP	84.7	63.0	73.9	6	1454.6	SEP	86.5	68.4	77.5	0	1449.4	SEP	54.4	34.4	44.4	618	709.4
OCT	75.8	50.8	63.3	137	1210.8	OCT	79.7	58.0	68.9	39	1298.7	OCT	33.5	16.9	25.2	1234	292.6
NOV	64.0	40.1	52.1	391	857.9	NOV	69.5	47.5	58.5	211	955.1	NOV	11.7	-6.2	2.8	1866	74.1
DEC	55.5	34.9	45.2	614	661.4	DEC	63.0	42.8	52.9	385	759.2	DEC	-1.5	-19.3	-10.4	2337	2.5
ANN	73.6	51.2	62.4	2844	1344.7	ANN	77.3	57.4	67.4	1684	1384.7	ANN	36.3	15.0	25.7	14344	767.8

Month	Normal Temperature (Deg F)*			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation Btu/ft ²	Month	Normal Temperature (Deg F)*			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation Btu/ft ²	Month	Normal Temperature (Deg F)*			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation Btu/ft ²
	Daily Max-min	Daily Min-max	Monthly				Base 65 Deg F Heating	Daily Max-min	Daily Min-max				Monthly	Base 65 Deg F Heating	Daily Max-min		
ARIZONA						CALIFORNIA (continued)						WASHINGTON, D.C.					
Phoenix Latitude 33° 26' N Elevation 1112'						San Francisco Latitude 37° 37' N Elevation 16'						Washington D.C. Latitude 38° 57' N Elevation 289'					
JAN	64.8	37.6	51.2	428	1021.3	JAN	55.3	41.2	48.3	518	707.6	JAN	41.2	23.0	32.1	1020	572.0
FEB	69.3	40.8	55.1	292	1374.1	FEB	58.6	43.8	51.2	386	1009.3	FEB	43.4	24.1	33.8	874	815.3
MAR	74.5	44.8	59.7	185	1814.1	MAR	61.0	44.9	53.0	372	1455.1	MAR	52.7	30.9	41.8	719	1125.0
APR	83.6	51.8	67.7	60	2354.8	APR	63.5	47.0	55.3	291	1920.0	APR	65.0	41.1	53.1	357	1458.9
MAY	92.9	59.6	76.3	0	2676.5	MAY	66.6	49.9	58.3	210	2225.6	MAY	74.5	50.6	62.6	131	1718.1
SEP	98.4	69.1	83.8	0	2015.4	SEP	73.6	54.5	64.1	66	1742.0	SEP	78.7	55.0	66.9	43	1340.0
OCT	87.6	56.8	72.2	17	1576.5	OCT	70.3	51.6	61.0	137	1226.1	OCT	68.2	43.5	55.9	291	1003.8
NOV	74.7	44.8	59.8	182	1150.5	NOV	63.3	47.2	55.3	291	821.4	NOV	55.6	33.7	44.7	609	650.9
DEC	66.4	38.5	52.5	388	932.0	DEC	56.3	42.9	49.7	474	642.2	DEC	43.3	24.7	34.0	961	481.1
ANN	85.1	55.4	70.3	1552	1869.4	ANN	65.1	48.7	56.9	3042	1552.8	ANN	64.7	42.7	53.7	5010	1208.4
Tucson Latitude 32° 07' N Elevation 2556'						COLORADO						FLORIDA					
JAN 63.5 38.2 50.9 442 1099.0						Denver Latitude 39° 45' N Elevation 5332'						Jacksonville Latitude 30° 30' N Elevation 29'					
FEB 67.0 39.9 53.5 333 1432.0						JAN 43.5 16.2 29.9 1088 840.1						JAN 64.6 44.5 54.6 348 899.9					
MAR 71.5 43.6 57.6 243 1864.3						FEB 46.2 19.4 32.8 902 1127.0						FEB 66.9 45.7 56.3 282 1164.3					
APR 80.7 50.3 65.5 81 2363.0						MAR 50.1 23.8 37.0 868 1530.4						MAR 72.2 50.1 61.2 176 1521.7					
MAY 89.6 57.5 73.6 0 2671.4						APR 61.0 33.9 47.5 525 1879.3						APR 79.0 57.1 68.1 24 1855.7					
SEP 93.1 67.1 80.1 0 1978.8						MAY 70.3 43.6 57.0 253 2134.9						MAY 84.6 63.9 74.3 0 1956.3					
OCT 83.8 56.4 70.1 29 1601.9						SEP 77.7 47.8 62.8 120 1726.8						SEP 86.0 70.4 78.2 0 1442.3					
NOV 72.2 44.8 58.5 221 1208.4						OCT 66.8 37.2 52.0 408 1300.5						OCT 79.2 61.7 70.5 19 1223.1					
DEC 64.8 39.1 52.0 403 995.8						NOV 53.3 25.4 39.4 768 883.5						NOV 71.4 51.0 61.2 161 996.0					
ANN 81.5 54.1 67.8 1752 1872.3						DEC 46.2 18.9 32.6 1004 731.8						DEC 65.6 45.1 55.4 317 817.6					
ARKANSAS						ANN 64.0 36.2 50.1 6016 1568.4						ANN 78.1 58.7 68.4 1327 1438.2					
Little Rock Latitude 34° 44' N Elevation 266'						CONNECTICUT						GEORGIA					
JAN 50.1 28.9 39.5 791 731.3						Hartford Latitude 41° 56' N Elevation 180'						Atlanta Latitude 33° 39' N Elevation 1033'					
FEB 53.8 31.9 42.9 619 1002.8						JAN 33.4 16.1 24.8 1246 477.5						JAN 51.4 33.4 42.4 701 717.6					
MAR 61.8 38.7 50.3 470 1312.7						FEB 35.7 17.9 26.8 1070 714.7						FEB 54.5 35.5 45.0 560 968.9					
APR 73.5 49.9 61.7 139 1610.7						MAR 44.6 26.6 35.6 911 978.5						MAR 61.1 41.1 51.1 443 1303.6					
MAY 81.4 58.1 69.8 21 1929.3						APR 58.9 36.5 47.7 519 1315.0						APR 71.4 50.7 61.1 144 1686.2					
SEP 85.8 60.8 73.3 5 1518.0						MAY 70.3 46.2 58.3 226 1568.5						MAY 79.0 59.2 69.1 27 1853.8					
OCT 76.0 48.7 62.4 143 1228.3						SEP 74.5 51.0 62.8 106 1154.5						SEP 81.2 63.4 72.3 8 1422.0					
NOV 62.4 38.1 50.3 441 847.2						OCT 64.3 40.8 52.6 384 852.9						OCT 72.5 52.3 62.4 137 1199.9					
DEC 51.2 31.1 41.6 725 673.7						NOV 50.6 31.9 41.3 711 497.3						NOV 61.9 40.8 51.4 408 882.9					
ANN 72.6 49.3 61.0 3354 1404.4						DEC 36.8 19.6 28.2 1141 385.1						DEC 52.7 34.3 43.5 667 674.2					
CALIFORNIA						ANN 59.6 38.6 49.1 6350 1058.3						ANN 70.3 51.3 60.8 3095 1345.3					
Los Angeles Latitude 33° 56' N Elevation 105'						DELAWARE						IDAHO					
JAN 63.5 45.4 54.5 331 926.1						Wilmington Latitude 39° 40' N Elevation 79'						Boise Latitude 43° 34' N Elevation 2868'					
FEB 64.1 47.0 55.6 270 1214.0						JAN 40.2 23.8 32.0 1023 571.4						JAN 36.5 21.4 29.0 1116 485.3					
MAR 64.3 48.6 56.5 267 1618.7						FEB 42.2 24.9 33.6 879 827.0						FEB 43.8 27.2 35.5 826 839.7					
APR 65.9 51.7 58.8 195 1950.9						MAR 51.1 32.0 41.6 725 1149.2						MAR 51.6 30.5 41.1 741 1304.1					
MAY 68.4 55.3 61.9 114 2059.6						APR 63.0 41.5 52.3 381 1480.1						APR 61.4 36.5 49.0 480 1826.9					
SEP 75.7 61.6 68.7 23 1681.4						MAY 73.1 51.6 62.4 128 1710.2						MAY 70.6 44.1 57.4 252 2276.7					
OCT 72.9 57.5 65.2 77 1317.0						SEP 78.2 57.6 67.9 32 1317.7						SEP 77.6 48.5 63.1 127 1737.2					
NOV 69.6 51.3 60.5 158 1003.9						OCT 67.8 46.5 57.2 254 983.9						OCT 64.7 39.4 52.1 406 1137.8					
DEC 66.5 47.3 56.9 279 848.5						NOV 55.2 36.2 45.7 579 644.6						NOV 48.9 30.7 39.8 756 628.3					
ANN 69.2 54.1 61.7 1819 1593.8						DEC 43.0 26.3 34.7 939 488.6						DEC 39.1 25.0 32.1 1020 437.2					
SACRAMENTO Latitude 38° 31' N Elevation 26'						ANN 63.7 44.3 54.0 4940 1207.7						ANN 62.6 39.1 50.9 5833 1495.5					
JAN 53.0 37.1 45.1 617 596.9																	
FEB 59.1 40.4 49.8 426 939.4																	
MAR 64.1 41.9 53.0 372 1458.4																	
APR 71.3 45.3 58.3 227 2003.6																	
MAY 78.8 49.8 64.3 120 2434.8																	
SEP 87.7 55.3 71.5 5 1906.7																	
OCT 77.1 49.5 63.3 101 1314.9																	
NOV 63.6 42.4 53.0 360 781.9																	
DEC 53.3 38.3 45.8 595 338.4																	
ANN 73.2 47.4 60.3 2843 1642.9																	

*Based on 1941-1970 Period. Zeros appearing for all values appearing in these columns signify that 1941-1970 period normals were not available.

Month	Normal Temperature (Deg F)			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F)			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F)			Normal Degree Days*	Total Hemispheric Mean Daily Solar Radiation			
	Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly			Daily Maximum	Daily Minimum	Monthly
	Base 65 Deg F Heating		DuB*				Base 65 Deg F Heating		DuB*				Base 65 Deg F Heating		DuB*			Base 65 Deg F Heating		DuB*
ILLINOIS						KANSAS (continued)						MARYLAND								
Chicago Latitude 41° 47' N Elevation 623'						Wichita Latitude 37° 39' N Elevation 1339'						Baltimore Latitude 39° 11' N Elevation 154'								
JAN	31.5	17.0	24.3	1262	507.0	JAN	41.4	21.2	31.3	1045	783.9	JAN	41.9	24.9	33.4	980	586.9			
FEB	34.6	20.2	27.4	1053	759.5	FEB	47.1	25.4	36.3	804	1058.2	FEB	43.9	25.7	34.8	846	840.0			
MAR	44.6	29.0	36.8	874	1106.9	MAR	55.0	32.1	43.6	671	1405.5	MAR	53.0	32.5	42.8	688	1162.2			
APR	59.3	40.4	49.9	453	1459.0	APR	68.1	45.1	56.6	275	1782.5	APR	65.2	42.4	53.8	340	1487.9			
MAY	70.3	49.7	60.0	208	1788.9	MAY	77.1	55.0	66.1	90	2035.8	MAY	74.8	52.5	63.7	110	1713.9			
SEP	75.8	56.0	65.9	57	1353.9	SEP	81.9	59.2	70.6	32	1616.1	SEP	79.0	57.9	68.5	27	1330.3			
OCT	65.0	45.6	55.4	316	968.9	OCT	71.3	47.9	59.6	211	1249.8	OCT	68.3	46.4	57.4	250	997.6			
NOV	48.1	32.6	40.4	738	565.6	NOV	55.8	33.8	44.8	606	870.8	NOV	56.1	36.0	46.1	567	660.3			
DEC	35.3	21.6	28.5	1132	401.5	DEC	44.3	24.6	34.5	946	689.9	DEC	43.9	26.6	35.3	921	499.3			
ANN	59.4	41.8	50.6	6127	1215.1	ANN	67.6	45.6	56.6	4687	1502.3	ANN	65.1	44.8	55.0	4729	1215.0			
INDIANA						KENTUCKY						MICHIGAN								
Indianapolis Latitude 39° 44' N Elevation 807'						Louisville Latitude 38° 11' N Elevation 489'						Detroit Latitude 42° 25' N Elevation 627'								
JAN	36.0	19.7	27.9	1150	495.6	JAN	42.0	24.5	33.3	983	545.5	JAN	31.7	19.2	25.5	1225	417.4			
FEB	39.3	22.1	30.7	960	746.9	FEB	45.0	26.5	35.8	818	789.3	FEB	33.7	20.1	26.9	1067	680.4			
MAR	49.0	30.3	39.7	784	1037.4	MAR	54.0	34.0	44.0	661	1102.0	MAR	43.1	27.6	35.4	918	1000.2			
APR	62.8	41.8	52.3	387	1398.4	APR	66.9	44.8	55.9	286	1466.7	APR	57.6	38.6	48.1	507	1399.0			
MAY	72.9	51.5	62.2	159	1688.0	MAY	75.6	53.9	64.8	105	1719.8	MAY	68.5	48.3	58.4	238	1715.9			
SEP	77.7	54.9	66.3	63	1324.0	SEP	80.5	57.7	69.1	35	1361.2	SEP	74.2	54.8	64.5	80	1253.2			
OCT	67.0	44.3	55.7	302	977.0	OCT	70.3	45.9	58.1	241	1042.2	OCT	63.4	45.2	54.3	342	876.1			
NOV	50.5	32.8	41.7	699	579.1	NOV	54.9	35.1	45.0	600	652.8	NOV	47.7	34.4	41.1	717	477.8			
DEC	38.7	23.1	30.9	1057	416.6	DEC	44.1	27.1	35.6	911	487.9	DEC	35.4	23.8	29.6	1097	343.5			
ANN	62.2	42.4	52.3	5577	1165.0	ANN	65.9	45.3	55.6	4645	1215.7	ANN	58.3	41.4	49.9	6228	1120.0			
LOUISIANA						MINNESOTA														
Baton Rouge Latitude 30° 32' N Elevation 75'						Duluth Latitude 46° 50' N Elevation 1417'														
JAN	61.5	40.5	51.0	451	785.1	JAN	17.6	-0.6	8.5	1751	388.6									
FEB	64.5	43.2	53.9	335	1054.1	FEB	22.1	2.0	12.1	1481	672.8									
MAR	70.6	48.7	59.7	208	1379.4	MAR	32.6	14.4	23.5	1287	1034.5									
APR	79.0	57.7	68.4	33	1681.2	APR	47.8	29.3	38.6	792	1372.8									
MAY	85.2	64.3	74.8	0	1871.2	MAY	60.0	38.8	49.4	484	1642.6									
SEP	87.2	67.7	77.5	0	1464.4	SEP	64.0	44.8	54.4	318	1095.0									
OCT	80.4	56.6	68.5	54	1301.1	OCT	54.3	36.2	45.3	611	724.8									
NOV	70.3	46.9	58.6	208	920.4	NOV	35.3	21.4	28.4	1098	380.7									
DEC	63.7	42.0	52.9	381	736.8	DEC	22.5	6.3	14.4	1569	291.7									
ANN	77.9	56.9	67.4	1670	1378.5	ANN	48.1	29.1	38.6	9756	1064.3									
MAINE						MISSISSIPPI														
Portland Latitude 43° 39' N Elevation 62'						Jackson Latitude 31° 29' N Elevation 331'														
JAN	31.2	11.7	21.5	1349	450.3	JAN	58.4	35.8	47.1	569	753.5									
FEB	33.3	12.5	22.9	1179	681.9	FEB	61.7	37.8	49.8	442	1026.4									
MAR	40.8	22.8	31.8	1029	969.6	MAR	68.7	43.4	56.1	313	1369.1									
APR	52.8	32.5	42.7	669	1303.9	APR	78.2	53.1	65.7	74	1708.4									
MAY	63.6	41.7	52.7	381	1567.4	MAY	85.0	60.4	72.7	6	1940.8									
SEP	69.9	47.4	58.7	200	1157.8	SEP	88.0	64.0	76.0	0	1509.2									
OCT	60.2	38.0	49.1	493	822.4	OCT	80.1	51.5	65.8	91	1271.4									
NOV	47.5	29.7	38.6	792	459.3	NOV	68.5	42.0	55.3	301	901.6									
DEC	34.9	16.4	25.7	1218	362.9	DEC	60.5	37.3	48.9	504	708.8									
ANN	55.3	34.7	45.0	7498	1050.6	ANN	77.1	52.8	65.0	2300	1408.6									
MASSACHUSETTS																				
Boston Latitude 42° 22' N Elevation 16'																				
JAN	35.9	22.5	29.2	1110	475.5															
FEB	37.5	23.3	30.4	969	709.6															
MAR	44.6	31.5	38.1	834	1016.4															
APR	56.3	40.8	48.6	492	1325.8															
MAY	67.1	50.1	58.6	218	1620.5															
SEP	72.2	56.7	64.5	76	1259.9															
OCT	63.2	47.5	55.4	301	889.6															
NOV	51.7	38.7	45.2	594	502.9															
DEC	39.3	26.6	33.0	992	403.0															
ANN	58.7	43.8	51.3	5621	1104.7															

Month	Normal Temperature (Deg F)°			Normal Degree Days°	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F)°			Normal Degree Days°	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F)°			Normal Degree Days°	Total Hemispheric Mean Daily Solar Radiation
	Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly				Daily Maximum	Daily Minimum	Monthly		
MISSOURI						NEVADA						NEW YORK					
Kansas City Latitude 39° 18' N Elevation 1033'						Las Vegas Latitude 36° 05' N Elevation 2178'						Albany Latitude 42° 45' N Elevation 292'					
JAN	35.7	18.4	27.1	1175	647.9	JAN	55.7	32.6	44.2	645	978.0	JAN	30.4	12.5	21.5	1349	456.5
FEB	41.4	23.1	32.3	916	894.7	FEB	61.3	36.9	49.1	451	1339.5	FEB	32.7	14.3	23.5	1162	688.4
MAR	50.7	30.6	40.7	753	1202.9	MAR	67.8	41.7	54.8	324	1823.5	MAR	42.6	24.2	33.4	980	985.9
APR	64.7	43.7	54.2	336	1575.0	APR	77.5	50.0	63.8	126	2319.0	APR	58.0	35.7	46.9	543	1335.2
MAY	74.2	54.0	64.1	127	1872.6	MAY	87.5	59.0	73.3	10	2646.3	MAY	69.7	45.7	57.7	253	1569.9
SEP	78.8	57.1	68.0	50	1452.4	SEP	94.8	65.4	80.1	0	2037.3	SEP	73.7	50.1	61.9	135	1170.3
OCT	68.2	46.9	57.6	259	1092.3	OCT	81.0	53.1	67.1	74	1539.8	OCT	62.8	40.0	51.4	422	817.3
NOV	51.4	33.1	42.3	681	737.3	NOV	65.7	40.8	53.3	357	1085.5	NOV	48.1	31.1	39.6	762	457.1
DEC	39.3	23.3	31.3	1045	561.5	DEC	56.7	33.7	45.2	614	880.5	DEC	34.1	17.7	25.9	1212	355.9
ANN	63.5	43.8	53.7	5357	1340.0	ANN	79.2	52.2	65.8	2601	1864.2	ANN	58.1	37.1	47.6	6888	1065.8
St. Louis Latitude 38° 45' N Elevation 564'						Reno Latitude 39° 30' N Elevation 4400'						Buffalo Latitude 42° 56' N Elevation 785'					
JAN	39.9	22.6	31.3	1045	627.4	JAN	45.4	18.3	31.9	1026	800.4	JAN	29.8	17.6	23.7	1280	348.9
FEB	44.2	26.0	35.1	837	885.6	FEB	51.1	23.0	37.1	781	1149.9	FEB	31.0	17.7	24.4	1137	546.4
MAR	53.0	33.5	43.3	682	1204.7	MAR	56.0	24.6	40.3	766	1649.4	MAR	39.0	25.2	32.1	1020	888.5
APR	67.0	46.0	56.5	272	1564.2	APR	64.0	29.6	46.8	546	2159.3	APR	53.3	36.4	44.9	603	1314.9
MAY	76.0	55.5	65.8	103	1871.3	MAY	72.2	37.0	54.6	328	2523.1	MAY	64.3	45.9	55.1	321	1596.5
SEP	80.1	59.1	69.6	35	1459.2	SEP	81.8	38.6	60.2	168	1997.7	SEP	70.8	52.3	61.6	138	1151.8
OCT	69.8	48.4	59.1	224	1099.8	OCT	70.0	30.5	50.3	456	1431.0	OCT	60.2	42.7	51.5	419	784.4
NOV	54.1	35.9	45.0	600	718.3	NOV	56.3	23.9	40.1	747	912.3	NOV	46.1	33.5	39.8	756	403.3
DEC	42.7	26.5	34.6	942	530.6	DEC	46.4	19.6	33.0	992	705.5	DEC	33.6	22.2	27.9	1150	283.3
ANN	65.6	46.2	55.9	4750	1326.6	ANN	67.0	31.7	49.4	6022	1760.7	ANN	55.0	39.1	47.1	6927	1034.3
MONTANA						NEW HAMPSHIRE						NEW YORK CITY					
Billings Latitude 45° 48' N Elevation 3570'						Concord Latitude 43° 12' N Elevation 344'						New York City Latitude 40° 47' N Elevation 187'					
JAN	31.2	12.5	21.9	1336	486.0	JAN	31.3	9.9	20.6	1376	459.5	JAN	38.5	25.9	32.2	1017	500.4
FEB	37.1	17.7	27.4	1054	763.0	FEB	33.8	11.3	22.6	1187	686.1	FEB	40.2	26.5	33.4	885	721.0
MAR	42.1	23.1	32.6	1004	1189.5	MAR	42.4	22.1	32.3	1014	973.6	MAR	48.4	33.7	41.1	741	1037.1
APR	55.8	33.4	44.6	612	1526.3	APR	56.7	31.7	44.2	624	1317.1	APR	60.7	43.5	52.1	387	1363.9
MAY	65.7	43.3	54.5	333	1912.8	MAY	68.6	41.5	55.1	315	1582.2	MAY	71.4	53.1	62.3	137	1636.2
SEP	71.3	46.5	58.9	221	1470.0	SEP	72.4	46.5	59.5	182	1140.2	SEP	76.8	59.9	68.4	29	1213.7
OCT	61.0	37.5	49.3	487	986.8	OCT	62.3	36.3	49.3	487	817.1	OCT	66.8	50.6	58.7	209	895.3
NOV	45.0	26.4	35.7	879	561.4	NOV	47.9	28.1	38.0	810	462.7	NOV	54.0	40.8	47.4	528	532.9
DEC	35.8	17.7	26.8	1184	421.2	DEC	34.6	14.9	24.8	1246	362.1	DEC	41.4	29.5	35.5	915	404.0
ANN	57.3	35.3	46.3	7265	1324.7	ANN	57.5	33.7	45.6	7360	1053.0	ANN	62.3	46.7	54.5	4848	1098.9
Great Falls Latitude 47° 28' N Elevation 3661'						NEW JERSEY						NORTH CAROLINA					
JAN	29.3	11.6	20.5	1380	420.5	Newark Latitude 40° 42' N Elevation 29'						Charlotte Latitude 35° 13' N Elevation 768'					
FEB	35.9	17.2	26.6	1075	720.2	JAN	38.5	24.3	31.4	1042	551.7	JAN	52.1	32.1	42.1	710	719.0
MAR	40.4	20.6	30.5	1070	1170.4	FEB	40.2	24.9	32.6	907	793.0	FEB	54.9	33.1	44.0	588	971.0
APR	54.5	32.3	43.4	648	1488.7	MAR	48.8	32.4	40.6	756	1108.7	MAR	62.2	39.0	50.6	461	1317.5
MAY	65.0	41.5	53.3	367	1847.6	APR	61.2	42.2	51.7	399	1448.6	APR	72.7	48.9	60.8	145	1695.0
SEP	70.0	44.6	57.3	260	1378.5	MAY	71.6	52.1	61.9	143	1687.1	MAY	82.0	57.4	68.8	34	1855.6
OCT	59.4	37.1	48.3	524	924.6	SEP	77.0	58.6	67.8	34	1272.9	SEP	80.2	61.9	72.0	10	1415.6
NOV	43.4	25.7	34.6	912	497.6	OCT	66.9	48.1	57.5	243	950.9	OCT	73.1	50.3	61.7	152	1173.4
DEC	34.7	18.2	26.5	1194	336.2	NOV	54.2	38.2	46.2	564	596.2	NOV	62.4	39.6	51.0	420	865.5
ANN	55.9	33.8	44.9	7652	1262.3	DEC	41.5	27.4	34.5	946	454.4	DEC	52.5	32.4	42.5	698	672.4
NEBRASKA						NEW MEXICO						Raleigh-Durham Latitude 35° 52' N Elevation 440'					
North Omaha Latitude 41° 22' N Elevation 1325'						Albuquerque Latitude 35° 03' N Elevation 5312'						JAN					
JAN	29.1	11.2	20.2	1389	634.0	JAN	46.9	23.5	35.2	924	1016.5	JAN	51.0	30.0	40.5	760	693.9
FEB	34.8	16.1	25.5	1106	892.1	FEB	52.6	27.4	40.0	700	1342.0	FEB	53.2	31.1	42.2	638	943.1
MAR	44.1	25.1	34.6	942	1222.5	MAR	59.2	32.3	45.8	595	1767.6	MAR	61.0	37.4	49.2	502	1275.1
APR	61.0	38.9	50.0	456	1558.4	APR	70.1	41.4	55.8	282	2228.4	APR	72.2	46.7	59.5	180	1644.3
MAY	71.4	50.4	60.9	186	1872.6	MAY	79.9	50.7	65.3	58	2538.1	MAY	79.4	55.4	67.4	48	1808.3
SEP	75.2	53.6	64.4	99	1373.2	SEP	83.4	56.7	70.1	7	1971.7	SEP	81.5	59.7	70.6	12	1377.1
OCT	65.9	42.8	54.4	342	1049.8	OCT	71.7	44.7	58.2	218	1546.7	OCT	72.4	48.0	60.2	186	1105.4
NOV	47.4	28.3	37.9	813	644.1	NOV	57.1	31.8	44.5	615	1133.7	NOV	62.1	37.8	50.0	450	812.1
DEC	34.3	17.0	25.7	1218	511.2	DEC	47.5	24.9	36.2	893	927.7	DEC	51.9	30.5	41.2	738	635.6
ANN	59.4	39.3	49.4	6601	1320.5	ANN	70.0	43.5	56.8	4292	1827.5	ANN	70.4	47.8	59.1	3514	1295.5

Month	Normal Temperature (Deg F) ^a			Normal Degree Days ^a	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F) ^a			Normal Degree Days ^a	Total Hemispheric Mean Daily Solar Radiation	Month	Normal Temperature (Deg F) ^a			Normal Degree Days ^a	Total Hemispheric Mean Daily Solar Radiation
	Daily Max-min	Daily Min-min	Monthly	Base 65 Deg F Heating	Btu/°F		Daily Max-min	Daily Min-min	Monthly	Base 65 Deg F Heating	Btu/°F		Daily Max-min	Daily Min-min	Monthly	Base 65 Deg F Heating	Btu/°F
TENNESSEE						TEXAS (continued)						WASHINGTON					
Knoxville Latitude 35° 49' N Elevation 981'						Lubbock Latitude 33° 39' N Elevation 3242'						Seattle-Tacoma Latitude 47° 27' N Elevation 400'					
JAN	48.9	32.2	40.6	756	620.7	JAN	53.4	24.8	39.1	803	1030.9	JAN	43.4	33.0	38.2	831	261.7
FEB	52.0	33.5	42.8	630	863.4	FEB	57.0	28.3	42.7	624	1331.7	FEB	48.5	36.0	42.3	636	495.0
MAR	60.4	39.4	49.9	484	1190.8	MAR	63.8	34.0	48.9	508	1762.0	MAR	51.5	36.6	44.1	648	849.0
APR	72.0	48.6	60.3	173	1598.9	APR	74.8	45.1	60.0	190	2167.8	APR	57.0	40.3	48.7	489	1293.5
MAY	79.8	56.9	68.4	47	1803.3	MAY	82.5	54.5	68.5	29	2395.9	MAY	64.1	45.6	54.9	313	1713.9
SEP	82.0	61.2	71.6	10	1383.2	SEP	83.8	58.2	71.0	8	1820.1	SEP	68.7	50.4	59.6	170	1147.7
OCT	71.8	50.0	60.9	175	1120.9	OCT	74.7	47.3	61.0	162	1468.2	OCT	59.4	44.9	52.2	397	656.2
NOV	58.9	39.4	49.2	474	758.7	NOV	63.1	34.4	48.8	486	1116.1	NOV	50.4	38.8	44.6	612	337.2
DEC	49.8	33.1	41.5	729	569.4	DEC	55.2	27.4	41.3	735	934.5	DEC	45.4	35.5	40.5	760	211.1
ANN	69.8	49.5	59.7	3478	1273.4	ANN	73.6	45.8	59.7	3545	1766.0	ANN	58.8	43.3	51.1	5185	1052.7
Memphis Latitude 35° 03' N Elevation 285'						UTAH						Spokane Latitude 47° 38' N Elevation 2366'					
JAN	49.4	31.6	40.5	760	682.7	JAN	37.4	18.5	28.0	1147	639.1	JAN	31.1	19.6	25.4	1228	315.0
FEB	53.1	34.4	43.8	594	944.8	FEB	43.4	23.3	33.4	885	988.7	FEB	39.0	25.3	32.2	918	605.9
MAR	60.8	41.1	51.0	457	1278.1	MAR	50.8	28.3	39.6	787	1454.3	MAR	46.2	28.8	37.5	853	1040.6
APR	72.7	52.3	62.5	131	1638.7	APR	61.8	36.6	49.2	474	1894.3	APR	57.0	35.2	46.1	567	1494.9
MAY	81.2	60.6	70.9	22	1884.9	MAY	72.4	44.2	58.3	237	2362.4	MAY	66.5	42.8	54.7	327	1918.0
SEP	84.3	62.8	73.6	7	1470.9	SEP	80.3	49.3	64.8	105	1843.3	SEP	72.5	46.7	59.6	196	1435.3
OCT	74.9	51.1	63.0	142	1204.5	OCT	66.4	38.4	52.4	402	1293.3	OCT	58.1	37.5	47.8	533	840.9
NOV	61.5	40.3	50.9	423	816.7	NOV	50.0	28.1	39.1	777	787.9	NOV	41.8	29.2	35.5	885	397.7
DEC	51.7	33.7	42.7	691	628.6	DEC	39.0	21.5	30.3	1076	569.8	DEC	33.9	24.0	29.0	1116	255.2
ANN	71.7	51.5	61.6	3227	1365.9	ANN	63.8	38.2	51.0	5983	1603.1	ANN	57.2	37.3	47.3	6835	1223.8
Nashville Latitude 36° 07' N Elevation 590'						VERMONT						WEST VIRGINIA					
JAN	47.6	29.0	38.3	828	579.6	JAN	25.9	7.6	16.8	1494	385.3	JAN	43.6	25.3	34.5	946	498.4
FEB	50.9	31.0	41.0	672	823.8	FEB	28.2	8.9	18.6	1299	606.8	FEB	46.2	26.8	36.5	798	706.5
MAR	59.2	38.1	48.7	524	1129.8	MAR	38.0	20.1	29.1	1113	940.2	MAR	55.2	33.8	44.5	642	1009.5
APR	71.3	48.8	60.1	176	1543.6	APR	53.3	32.6	43.0	660	1296.2	APR	67.9	43.8	55.9	287	1355.7
MAY	79.8	57.3	68.5	45	1824.8	MAY	66.1	43.5	54.8	331	1574.1	MAY	76.6	52.3	64.5	113	1639.4
SEP	83.5	60.5	72.0	10	1397.9	SEP	70.0	48.6	59.3	191	1122.2	SEP	79.0	55.9	67.5	46	1272.0
OCT	73.2	48.6	60.9	190	1113.8	OCT	58.7	38.8	48.8	502	740.5	OCT	69.1	44.8	57.0	267	972.3
NOV	59.0	37.7	48.4	498	711.3	NOV	44.3	29.7	37.0	840	374.6	NOV	55.8	35.0	45.4	588	613.1
DEC	49.6	31.1	40.4	763	520.6	DEC	30.3	14.8	22.6	1314	283.2	DEC	45.2	27.2	36.2	893	440.1
ANN	70.1	48.7	59.4	3696	1269.7	ANN	54.2	34.5	44.4	7876	1020.7	ANN	66.0	44.4	55.2	4590	1123.3
TEXAS						VIRGINIA						WISCONSIN					
Dallas Latitude 32° 51' N Elevation 489'						Richmond Latitude 37° 30' N Elevation 164'						Milwaukee Latitude 42° 57' N Elevation 492'					
JAN	55.1	35.7	45.4	608	821.5	JAN	47.4	27.6	37.5	853	631.9	JAN	27.3	11.4	19.4	1414	479.4
FEB	59.2	39.5	49.4	437	1071.1	FEB	49.9	28.8	39.4	717	877.1	FEB	30.3	14.6	22.5	1190	736.5
MAR	66.4	45.2	55.8	314	1421.8	MAR	58.2	35.5	46.9	569	1210.4	MAR	39.4	23.4	31.4	1042	1088.8
APR	76.3	56.4	66.4	71	1626.8	APR	70.3	45.2	57.8	226	1566.0	APR	54.6	34.7	44.7	609	1442.7
MAY	83.1	64.4	73.8	0	1888.5	MAY	78.4	54.5	66.5	64	1762.0	MAY	65.0	43.3	54.2	348	1768.4
SEP	88.0	68.3	78.2	0	1587.1	SEP	80.9	59.0	70.0	21	1347.9	SEP	71.5	50.7	61.1	140	1310.3
OCT	78.4	57.5	68.0	55	1276.1	OCT	71.2	47.4	59.3	203	1032.7	OCT	61.4	40.6	51.0	440	907.9
NOV	66.4	45.4	55.9	284	936.4	NOV	60.6	37.3	49.0	480	733.0	NOV	44.4	28.5	36.5	855	524.6
DEC	57.8	38.6	48.2	521	780.1	DEC	49.1	28.8	39.0	806	566.7	DEC	31.5	16.8	24.2	1265	378.4
ANN	76.0	56.3	66.2	2290	1468.1	ANN	68.8	46.7	57.8	3939	1248.0	ANN	55.1	36.3	45.7	7444	1191.2
El Paso Latitude 31° 48' N Elevation 3917'						Roanoke Latitude 37° 19' N Elevation 1174'						WYOMING					
JAN	57.0	30.2	43.6	663	1125.1	JAN	45.6	27.2	36.4	887	660.5	JAN	38.2	14.9	26.6	1190	765.8
FEB	62.5	34.3	48.4	465	1480.1	FEB	47.9	28.3	38.1	753	899.4	FEB	40.7	17.3	29.0	1088	1067.8
MAR	68.9	40.3	54.6	328	1909.3	MAR	56.3	34.3	45.3	611	1236.1	MAR	43.5	19.6	31.6	1035	1433.1
APR	78.5	49.3	63.9	89	2363.5	APR	67.9	43.9	55.9	283	1581.5	APR	55.4	30.0	42.7	669	1770.5
MAY	87.2	57.2	72.2	0	2600.6	MAY	76.1	52.7	64.4	101	1763.9	MAY	65.1	39.7	52.4	394	1994.6
SEP	87.4	61.0	74.2	0	1987.1	SEP	79.5	56.5	68.0	32	1358.2	SEP	72.8	43.5	58.2	225	1667.4
OCT	78.5	49.5	64.0	92	1639.0	OCT	69.9	45.6	57.8	235	1080.2	OCT	61.8	33.9	45.5	530	1241.8
NOV	66.1	37.0	51.6	402	1243.7	NOV	57.6	35.8	46.7	549	764.7	NOV	47.5	23.5	35.5	885	822.8
DEC	57.8	30.9	44.4	639	1030.7	DEC	46.6	28.1	37.4	856	590.8	DEC	40.3	18.1	29.2	1110	671.0
ANN	77.2	49.5	63.4	2678	1899.7	ANN	66.8	45.0	55.9	4307	1269.5	ANN	58.9	33.0	45.9	7255	1490.7

^a Reprinted from the U.S. Department of Commerce, National Oceanic and Atmospheric Administration, Environmental Data and Information Service, National Climate Center, Asheville, North Carolina - "Input Data for Solar Systems," by V. V. Cinquemani, J. R. Owenby, Jr., and R. G. Baldwin.

^b Based on 1941 - 1970 Period. Zeros appearing for all values appearing in these columns signify that 1941 - 1970 period normals were not available.

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Projection greater than 20 ft required.